



Fig. 3 (a) A  $p-n-p$  transistor connected in common-base configuration for amplifier application. (b) Doping profiles of a transistor with abrupt impurity distributions. (c) Energy-band diagram under normal operating conditions.

where  $n_E$  is the equilibrium minority-carrier density (electrons) in the emitter. A similar set of equations can be written for the collector junction:

$$p'(W) = p(W) - p_B = p_B \left[ \exp\left(\frac{qV_{CB}}{kT}\right) - 1 \right] \quad (4)$$

$$n'(x_C) = n(x_C) - n_C = n_C \left[ \exp\left(\frac{qV_{CB}}{kT}\right) - 1 \right].$$

The solutions for the minority-carrier distributions, that is, the hole distribution in the base from Eq. 1 and electron distributions in the emitter

and collector, are given by

$$p(x) = p_B + \left[ \frac{p'(W) - p'(0)e^{-W/L_B}}{2 \sinh(W/L_B)} \right] e^{x/L_B} - \left[ \frac{p'(W) - p'(0)e^{W/L_B}}{2 \sinh(W/L_B)} \right] e^{-x/L_B} \quad (5)$$

$$n(x) = n_E + n'(-x_E) \exp\left[\frac{(x + x_E)}{L_E}\right], \quad x < -x_E \quad (6)$$

$$n(x) = n_C + n'(x_C) \exp\left[-\frac{(x - x_C)}{L_C}\right], \quad x > x_C \quad (7)$$

where  $L_B = \sqrt{\tau_B D_B}$  is the diffusion length of holes in the base, and  $L_E$  and  $L_C$  are the diffusion lengths in the emitter and collector, respectively. Equation 5 is important because it correlates the base width  $W$  to the minority-carrier distribution. If  $W \rightarrow \infty$  or  $W/L_B \gg 1$ , Eq. 5 reduces to

$$p(x) = p_B + p(0)e^{-x/L_B} \quad (8)$$

which is identical to the case of a  $p-n$  junction. In this case, there is no communication between the emitter and collector currents, which are determined by the density gradient at  $x = 0$  and  $x = W$ , respectively. The "transistor" action is thus lost. From Eqs. 2 and 3 we can obtain the total dc emitter current as a function of the applied voltages:

$$\begin{aligned} I_E &= AJ_p(x=0) + AJ_n(x=-x_E) \\ &= A \left( -qD_B \frac{\partial p}{\partial x} \Big|_{x=0} \right) + A \left( -qD_E \frac{\partial n}{\partial x} \Big|_{x=-x_E} \right) \\ &= Aq \frac{D_B p_B}{L_B} \coth\left(\frac{W}{L_B}\right) \left[ (e^{qV_{EB}/kT} - 1) - \frac{1}{\cosh(W/L_B)} (e^{qV_{CB}/kT} - 1) \right] \\ &\quad + Aq \frac{D_E n_E}{L_E} (e^{qV_{EB}/kT} - 1) \end{aligned} \quad (9)$$

and for the total dc collector current

$$\begin{aligned} I_C &= AJ_p(x=W) + AJ_n(x=x_C) \\ &= A \left( -qD_B \frac{\partial p}{\partial x} \Big|_{x=W} \right) + A \left( -qD_C \frac{\partial n}{\partial x} \Big|_{x=x_C} \right) \\ &= Aq \frac{D_B p_B}{L_B} \frac{1}{\sinh(W/L_B)} \left[ (e^{qV_{EB}/kT} - 1) - \coth\left(\frac{W}{L_B}\right) (e^{qV_{CB}/kT} - 1) \right] \\ &\quad - Aq \frac{D_C n_C}{L_C} (e^{qV_{CB}/kT} - 1) \end{aligned} \quad (10)$$

where  $A$  is the cross-sectional area of the transistor. The difference between these two currents is small and appears as the base current:

$$I_B = I_E - I_C. \quad (11)$$

We shall now modify the doping distribution in the base layer of Fig. 3b