

Prob. 6.1

Find V_O , V_P , and V_T . Find $V_{D,sat}$ for $V_G = -3V$.

$$V_O = \frac{kT}{q} \cdot \ln \frac{N_a \cdot N_d}{n_i^2} = 0.0259 \text{eV} \cdot \ln \frac{10^{18} \frac{1}{\text{cm}^3} \cdot 10^{16} \frac{1}{\text{cm}^3}}{\left(1.5 \cdot 10^{10} \frac{1}{\text{cm}^3}\right)^2} = 0.814 \text{V}$$

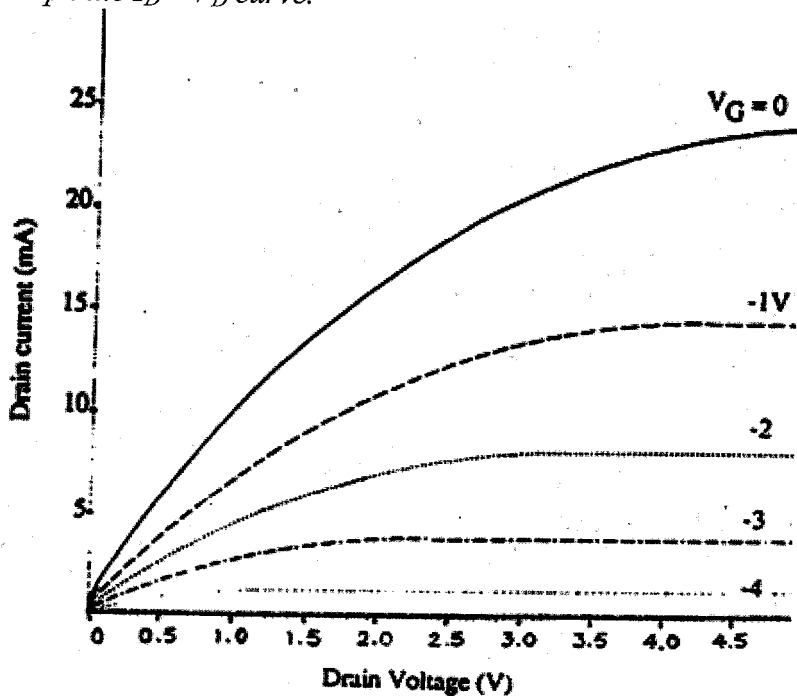
$$V_P = \frac{q \cdot a^2 \cdot N_d}{2 \cdot \epsilon} = \frac{1.6 \cdot 10^{-19} \text{C} \cdot (10^{-4} \text{cm})^2 \cdot 10^{16} \frac{1}{\text{cm}^3}}{2 \cdot 11.8 \cdot 8.85 \cdot 10^{16} \frac{\text{F}}{\text{cm}}} = 7.66 \text{V}$$

$$V_T = V_P - V_O = 6.85 \text{V}$$

$$V_{D,sat} = V_T + V_G = 6.85 \text{V} - 3.00 \text{V} = 3.85 \text{V}$$

Prob. 6.4

Graph the $I_D - V_D$ curve.



Prob. 6.6

For current I_D varying linearly with V_D at low values of V_D for a JFET,
(a) use the binomial expansion to rewrite Equation 6-9

Equation 6-9 may be rewritten as

$$I_D \approx G_O \cdot V_P \cdot \left[\frac{V_D}{V_P} + \frac{2}{3} \cdot \left(\frac{-V_G}{V_P} \right)^{\frac{3}{2}} - \frac{2}{3} \cdot \left(\frac{V_D - V_G}{V_P} \right)^{\frac{3}{2}} \right]$$

$$I_D = G_O \cdot \left[V_D + \frac{2}{3} \cdot \frac{(-V_G)^{\frac{3}{2}}}{V_P^{\frac{1}{2}}} - \frac{2}{3} \cdot \frac{(-V_G)^{\frac{3}{2}}}{V_P^{\frac{1}{2}}} \cdot \left(\frac{V_D}{-V_G} + 1 \right)^{\frac{3}{2}} \right]$$

use the binomial approximation $(1+x)^{\frac{3}{2}} \approx 1 + \frac{3}{2} \cdot x$

$$I_D = G_O \cdot \left[V_D + \frac{2}{3} \cdot \frac{(-V_G)^{\frac{3}{2}}}{V_P^{\frac{1}{2}}} - \frac{2}{3} \cdot \frac{(-V_G)^{\frac{3}{2}}}{V_P^{\frac{1}{2}}} \cdot \left(1 + \frac{3}{2} \cdot \left(-\frac{V_D}{V_G} \right) \right) \right]$$

$$I_D = G_O \cdot V_D \cdot \left[1 - \left(\frac{-V_G}{V_P} \right)^{\frac{1}{2}} \right]$$

(b) show that I_D/V_D in the linear range is the same as g_m (sat),

$$\frac{I_D}{V_D} = G_O \cdot \left[1 - \left(\frac{-V_G}{V_P} \right)^{\frac{1}{2}} \right] = g_m(\text{sat})$$

(c) and find the value of V_G for device turn off.

$$V_G = -V_P$$

Prob. 6.20

$$V_T = V_{FB} + 2\phi_F - \frac{Q_d}{C_i}$$

$$V_{FB} = 2\phi_F - \frac{Q_i}{C_i}$$

$$C_i = \frac{\epsilon_i}{d} = \frac{8.85 \times 10^{-14} \times 3.9}{100 \times 10^{-8}} = 3.452 \times 10^{-7} \text{ F/cm}^2$$

Note: Here we use dielectric constant of oxide.

According to Fig. (6-17) in the textbook, for $N_a = 10^{18} \text{ cm}^{-3}$

$$\Rightarrow \Phi_{ms} = -1.1 \text{ V}$$

$$V_{FB} = \Phi_{ms} - \frac{Q_i}{C_i} = -1.1 - \frac{5 \times 10^{10} \times 1.6 \times 10^{-19}}{3.452 \times 10^{-7}} = -1.12 \text{ V}$$

$$\phi_F = \frac{kT}{q} \ln \frac{N_a}{n_i} = 0.0259 \cdot \ln \left(\frac{10^{18}}{1.5 \times 10^{10}} \right) = 0.467 \text{ V}$$

$$W = \sqrt{\frac{2\epsilon_s(2\phi_F)}{qN_a}} = \sqrt{\frac{2(11.8)(8.85 \times 10^{-14})(2 \times 0.467)}{1.6 \times 10^{-19} \times 10^{18}}} = 3.49 \times 10^{-6} \text{ cm}$$

Note: Here we used dielectric constant of Si.

$$Q_d = -qN_a W_m$$

$$V_T = V_{FB} + 2\phi_F - \frac{Q_d}{C_i} = -1.12 + 2(0.467) + \frac{1.6 \times 10^{-19} \times 10^{18} \times 3.49 \times 10^{-6}}{3.452 \times 10^{-7}} = 1.43 \text{ V}$$

Prob. 6.21

For the MOSFET, calculate the drain current at $V_G = 5 \text{ V}$, $V_D = 0.1 \text{ V}$.

Repeat for $V_G = 3 \text{ V}$, $V_D = 5 \text{ V}$.

For $V_G = 5 \text{ V}$, $V_D = 0.1 \text{ V}$, since $V_T = 1 \text{ V}$

$V_D < (V_G - V_T) \rightarrow$ linear region

$$\begin{aligned} I_D &= \frac{Z}{L} \cdot \bar{\mu}_n \cdot C_i \cdot \left[(V_G - V_T) \cdot V_D - \frac{1}{2} \cdot V_D^2 \right] \\ &= \frac{50 \mu\text{m}}{2 \mu\text{m}} \cdot 200 \frac{\text{cm}^2}{\text{V}\cdot\text{s}} \cdot 3.452 \cdot 10^{-7} \text{ F} \cdot \left[(5 \text{ V} - 1 \text{ V}) \cdot 0.1 \text{ V} - \frac{1}{2} (0.1 \text{ V})^2 \right] = 6.82 \cdot 10^{-4} \text{ A} \end{aligned}$$

For $V_G = 3 \text{ V}$, $V_D = 5 \text{ V}$, $V_D(\text{sat}) = V_G - V_T = 3 \text{ V} - 1 \text{ V} = 2 \text{ V}$

$$\begin{aligned} I_D &= \frac{Z}{L} \cdot \bar{\mu}_n \cdot C_i \cdot \left[(V_G - V_T) \cdot V_D(\text{sat}) - \frac{1}{2} \cdot V_D^2(\text{sat}) \right] \\ &= \frac{50 \mu\text{m}}{2 \mu\text{m}} \cdot 200 \frac{\text{cm}^2}{\text{V}\cdot\text{s}} \cdot 3.452 \cdot 10^{-7} \text{ F} \cdot \left[(2 \text{ V})^2 - \frac{1}{2} (2 \text{ V})^2 \right] = 3.45 \cdot 10^{-3} \text{ A} \end{aligned}$$

Prob. 6.22

For the given MOSFET, calculate the linear V_T and k_N , saturation V_T and k_N .

1. Choose $V_D \ll V_D(\text{sat})$ to ensure that I_D - V_D curve is in the linear regime

e.g., choose $V_D = 0.2\text{V}$

(1)	$V_G = 4\text{ V}$	$V_D = 0.2\text{ V}$	$I_D = 0.35\text{ mA}$
(2)	$V_G = 5\text{ V}$	$V_D = 0.2\text{ V}$	$I_D = 0.62\text{ mA}$

In linear regime

(3) $I_D = k_N[(V_G - V_T)V_D - V_D^2/2]$

From equation (3), inserting the values from (1) and (2)

$$0.35 \cdot 10^{-3} = k_N [(4 - V_T)(0.2)]$$

$$0.62 \cdot 10^{-3} = k_N [(5 - V_T)(0.2)]$$

$$0.35/0.62 = (4 - V_T) / (5 - V_T)$$

$$1.75 - 0.35V_T = 2.48 - 0.62V_T$$

$$V_T = 2.71\text{V}, \text{ therefore, } k_N = 1.36 \cdot 10^{-3} \text{ A/V}^2$$

2. Choose $V_D \gg V_D(\text{sat})$ to ensure that I_D - V_D curve is in the saturation regime

e.g. choose $V_D = 3\text{V}$

(4)	$V_G = 4\text{ V}$	$V_D = 3\text{ V}$	$I_D = 0.74\text{ mA}$
(5)	$V_G = 5\text{ V}$	$V_D = 3\text{ V}$	$I_D = 1.59\text{ mA}$

In saturation regime

(6) $I_D = (1/2) k_N (V_G - V_T)^2$

$$0.74 \cdot 10^{-3} = \frac{k_N}{2} (4\text{V} - V_T)^2$$

$$1.59 \cdot 10^{-3} = \frac{k_N}{2} \cdot (5\text{V} - V_T)^2$$

$$\frac{0.74}{1.59} = \frac{(4\text{V} - V_T)^2}{(5\text{V} - V_T)^2}$$

$$V_T = 1.85\text{V}, \quad k_N = 3.20 \cdot 10^{-4} \text{ A/V}^2$$